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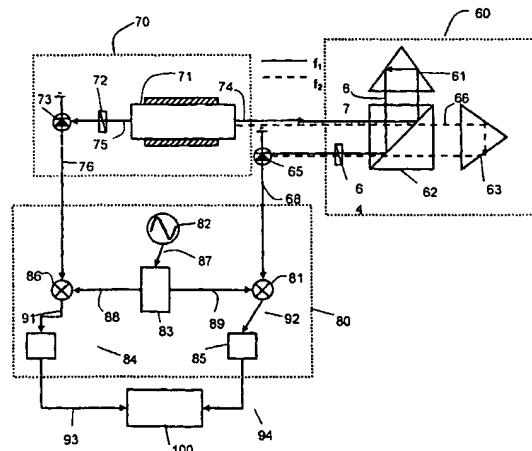
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(54) Title: HETERODYNE LASER INTERFEROMETER USING HETEROGENEOUS MODE HELIUM-NEON LASER AND SUPER HETERODYNE PHASE MEASURING METHOD



(57) Abstract: Disclosed are a method and a device for detecting the phase of a moving object using a heterodyne interferometer. A heterogeneous mode helium-neon laser is used in the heterodyne interferometer as a direct light source to increase a measuring speed and a measuring resolution performance as well as minimizing the loss of the light source. Signals, which have only a frequency difference between reference signals or measured signals and arbitrary signals, are extracted from signals which are obtained by multiplying the arbitrary frequency signals by the reference signals or the measured signals. After frequencies of the reference signals and the measured signals are converted, a phase difference of the extracted signals is measured, and a displacement of the moving object is measured. The laser interferometer system of the present invention includes a laser light source part, an optical interferometer, a frequency converter, and a phase measurer. The light source used in the heterodyne interferometer uses output light emitted from a heterogeneous mode helium-neon laser generator, which is stabilized in frequency, and such output light have two frequencies which are at right angles to each other and linearly polarized.

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HETERODYNE LASER INTERFEROMETER USING
HETEROGENEOUS MODE HELIUM-NEON LASER AND SUPER
HETERODYNE PHASE MEASURING METHOD

Technical Field

The present invention relates to a method and device for detecting displacement of a moving object using a heterodyne interferometer. Specifically, the invention relates to a method and device for detecting displacement of a moving object, which uses a heterogeneous mode helium-neon laser as a direct light source for a heterodyne interferometer to minimize the loss of the light source, extracts signals, which have only a frequency difference between reference signals or measured signals and arbitrary signals, from signals that are obtained by multiplying the arbitrary frequency signals by the reference signals or the measured signals to increase a measuring speed and a measuring resolution, converts frequencies of the reference signals and the measured signals, and then measures a phase difference of the extracted signals, thereby measuring the displacement of the moving object.

Background Art

First of all, the technique and principle of a conventional heterodyne displacement measuring interferometer will be explained hereinafter in order to improve the understanding of the present invention. The present technical situation of a laser light source of the

heterodyne interferometer is described first. As implied by the word " heterodyne" , a laser light source of the heterodyne interferometer must output light having two frequencies which are at right angles to each other and linearly polarized, as shown in FIG. 1. There are two typical methods for generating this light. The first one is a method using Zeeman effect, which applies a magnetic field to a gain material to generate two frequencies and the second one is a method using an acousto-optic modulator (hereinafter, referred to as " AOM").

Specifically, the first method applies a magnetic field to a laser operating in a single mode using Zeeman effect by which the spectrum of an atom is divided into two when a magnetic field is applied to the gain material, to thereby obtain light having two frequencies whose polarized beams are perpendicular to each other. This method can relatively easily construct a heterodyne light source. However, the maximum difference between the two frequencies is merely 3MHz so that the maximum measuring speed is limited to 475mm/s when a plane mirror interferometer is used.

The second method for obtaining a light source using an AOM became commercially available by Zygo, Co., of America. This method passes one of two frequencies of light that oscillate in a heterogeneous-mode laser through a polarizer and inputs the resultant frequencies to the AOM to obtain linearly polarized light having two frequency components with a frequency difference of 20MHz between them. The

light source obtained through this method has a high beat frequency so that a measuring band of the light source becomes larger than that of the light source acquired according to Zeeman effect. Furthermore, even in the case where the beat frequency is stabilized and the laser is changed into another one, the beat frequency can be controlled to be identical to the stabilized one. However, the loss of light is considerable because one of the two frequencies should pass through the polarizer. Moreover, a polarization prism cannot perfectly align two beams with one axis so that measurement becomes difficult when a measuring distance is longer than 10m.

Next, a phase measuring method and the technical situation of a conventional heterodyne interferometer will be explained. A phase measurer measures a frequency difference between a reference signal having a specific frequency and a measured signal obtained by adding Doppler frequency to the frequency of the reference signal according to movement of an object and continuously adds up the measured frequency difference, to detect the displacement of the moving object. When a reflecting mirror moves at a rate v , Doppler frequency Δf according to the movement of the reflecting mirror is represented by the following Expression.

$$\Delta f = 2nv(t)/\lambda \quad (\text{Expression 1})$$

Where, n is the refractive index of air and λ is wavelength of light. When the reflecting mirror moves at 1m/s, Doppler frequency caused by

the movement of the reflecting mirror is 3.16MHz. In case of a plane mirror interferometer where light reaches the reflecting mirror twice, Doppler frequency becomes 6.32MHz, which is twice the Doppler frequency of the above-described case. This means that 6.32×10^6 interference patterns pass for one second. The phase measurer must have a high frequency band so as not to miss the number of interference patterns.

The phase measurer mostly measures the ratio of the cycle of the reference signal to a zero crossing time difference of the reference signal and the measured signal, to obtain a phase value. The phase of the two signals is defined as follows.

$$\phi = 360^\circ \times \frac{T_+}{T_R} \quad (\text{Expression 2})$$

Where, T_R is the cycle of the reference signal V_R , and T_+ is the zero crossing time difference of the reference signal V_R and the measured signal V_m . The phase measurer counts internal clocks during T_+ and T_R to obtain the phase value. Accordingly, the resolution of the phase measurer is determined by the cycle of the reference signal and a time resolution of the phase measurer. That is, the following relationship is accomplished

$$\Delta\theta = 360^\circ f_R \Delta\tau \quad (\text{Expression 3})$$

Where, $\Delta\theta$ means an angle resolution of the phase measurer, f_R means the frequency of the reference signal, and $\Delta\tau$ is the time resolution of the phase measurer. According to the expression 3, the

phase resolution becomes 3.6° when the time resolution of the phase measurer is 1nsec and the frequency of the reference signal is 10MHz, and the phase resolution is 0.36° when the frequency of the reference signal is 1MHz. This means that the phase resolution increases as the frequency of the reference signal decreases. However, the phase resolution is limited by a measuring speed. In general, phase measurement is carried out for every one cycle of the reference signal so that the frequency of the reference signal becomes a sampling frequency of the phase value. When a phase variation is more than $2/3$ during one sampling period, phase unwrapping becomes difficult. This can be represented by the following Expression.

$$\Delta\phi < |2\pi/3| \quad (\text{Expression 4})$$

Where, $\Delta\phi$ is a phase variation during a sampling period.

The limit of measurable Doppler frequency Δf can be obtained when both sides of the expression 4 are divided by sampling time, that is, half the cycle of the reference signal.

$$|\Delta f| = \left| \frac{\Delta\phi}{2\pi(\frac{T_R}{2})} \right| < \frac{2}{3} f_R \quad (\text{Expression 5})$$

Where, f_R is the frequency of the reference signal, which is obtained through $f_1 - f_2$.

In the case where the frequency of the reference is 1MHz and the plane mirror interferometer is used, a maximum measurable movement

speed is approximately 104mm/s from the Expressions 1 and 5. Because a maximum movement speed is proportional to the frequency of the reference signal, the frequency of the reference signal should be increased in order to measure an object moving rapidly. In this case, however, resolution is decreased. The relationship between the measuring speed v and a length resolution ΔL is represented as follows.

$$\Delta \tau < 2\Delta \frac{L}{3v} \quad (\text{Expression 6})$$

The conventional phase measuring method must satisfy the relationship of the Expression 6. Accordingly, to increase the time resolution is the only way to improve both of the measuring speed and the measuring resolution. To obtain the resolution of 0.3mm at the movement speed of 2m/s, the time resolution of at least 100ps is needed. Thus, it is difficult and costly to obtain the resolution.

As described above, the conventional heterodyne interferometer has a large loss of light during generation of the light source so that the light source with high power is difficult to obtain. In addition, the time resolution should be increased in order to acquire a high measuring speed and measuring resolution in the conventional heterodyne interferometer. However, there are limits in the time resolution so that it is difficult to actually construct a laser interferometer system.

Disclosure Of The Invention

Accordingly, the present invention has been made in view of the above-mentioned problems, and it is an object of the present invention

is to provide a method and device for detecting displacement of a moving object using a heterodyne interferometer.

To accomplish the object of the present invention, the invention uses a heterogeneous mode helium-neon laser as a direct light source for a heterodyne interferometer to minimize the loss of the light source, extracts signals, which have only a frequency difference between reference signals or measured signals and arbitrary signals, from signals that are obtained by multiplying the arbitrary frequency signals by the reference signals or the measured signals to increase a measuring speed and a measuring resolution, converts frequencies of the reference signals and the measured signals, and then measures a phase difference of the extracted signals, thereby measuring the displacement of the moving object.

It is to be understood that both the foregoing general description and the following detailed description of the present invention are exemplary and explanatory and are intended to provide further explanation of the invention as claimed.

Brief Description of the Drawings

Further objects and advantages of the invention can be more fully understood from the following detailed description taken in conjunction with the accompanying drawings in which:

FIG.1 shows a conventional heterodyne displacement measuring interferometer;

FIG. 2 shows a gain curve of a heterogeneous mode HeNe laser;

FIG. 3 shows a heterodyne laser interferometer using a heterogeneous mode HeNe laser and a super heterodyne phase measuring method according to the present invention;

FIG. 4A shows a measuring band when a beat frequency is not decreased;

FIG. 4B shows a measuring band when Doppler frequency operates in positive and negative directions; and

FIG. 4C shows a configuration for canceling a measuring band in the negative direction in a two-way heterodyne interferometer.

Best mode for Carrying Out the Invention

Reference will now be made in detail to the preferred embodiments of the present invention, examples of which are illustrated in the accompanying drawings.

The laser interferometer system of the present invention includes a heterogeneous mode helium-neon laser source used in the interferometer, which is stabilized in frequency, an optical interferometer for generating an interference pattern, a detector for converting the interference pattern into an electric signal, and a phase measurer for measuring the phase of the signal obtained from the detector.

The heterogeneous mode helium-neon laser means a laser that has two modes 45 and 46 satisfying an ordinary wave condition of a

resonator whose length is 150 to 200mm on a gain curve 40 of helium-neon, as shown in FIG. 2, to output light having two frequencies. The distance between the two modes is determined by a free spectral range. The distance between the two modes depends on the length of the resonator but is in the range of 600 to 1000MHz in general. The two modes are perpendicular to each other and linearly polarized so that one mode is in P polarization state when the other mode is in S polarization state.

An embodiment of the heterodyne displacement measuring laser interferometer using the helium-neon laser according to the present invention will be explained below.

FIG. 3 shows the laser interferometer system of the present invention. The laser interferometer system includes a laser light source part 70, an optical interferometer 60, a frequency converter 80, and a phase measurer 90. The light source used in the heterodyne interferometer uses output light 74 emitted from a heterogeneous mode helium-neon laser generator 71. The output light has two frequencies that are at right angles to each other and linearly polarized. A part 75 of the output light passes through a polarizer 72 whose polarization axis is tilted at 45° to the light to interfere, to be used as a reference signal. The interference light passes through a photo-detector 73 to be converted into an electric signal 76. This electric signal is used as the reference signal to be compared with a measured signal that is inputted

to a moving object and outputted from the moving object. The reference signal is represented by the following Expression.

$$V_r = A \cos[2\pi(f_1 - f_2)t] \quad (\text{Expression 7})$$

Where, V_R means the reference signal, A denotes the amplitude of the signal, and f_1 and f_2 are frequency components included in the output light. The remaining output light 74 emitted from the laser generator 71 is inputted into a polarization splitter 62, which splits light according to a polarization direction, to be split so that light 67 having the frequency component f_1 travels to a fixed reflecting mirror 61 and light 66 having the frequency component f_2 travels to a moving reflecting mirror 63 attached to a moving object. The lights inputted into the fixed reflecting mirror and the moving reflecting mirror are reflected and combined by a polarizer 64 whose polarization axis is tilted at 45° to the lights to interfere with each other, and then inputted to a photo-detector 65. The light inputted into the photo-detector is converted into an electric signal 68, which is used as the measured signal. When the light having the frequency component f_1 has traveled by d_1 in the air, the actual light traveling path is $2nd_1$. When the beam having the frequency component f_2 has traveled by d_2 in the air, the light traveling path becomes $2nd_2$. Accordingly, the measured signal is represented as follows.

$$V_m = B \cos\{2\pi(f_1 - f_2)t + 2nd_1 / \lambda_1 - 2nd_2 / \lambda_2\} \quad (\text{Expression 8})$$

Where, V_m is the measured signal, B is the amplitude of the signal, n is the refractive index of air, and λ_1 and λ_2 mean wavelengths of the lights having the frequency components f_1 and f_2 , respectively.

Since the absolute phase value is not important in the interferometer, from the Expression 7 representing the reference signal and the Expression 8 representing the measured signal, a phase difference between the two signals is obtained as follows.

$$\phi \cong 4\pi n(d_1 - d_2) / \lambda_2 \quad (\text{Expression 9})$$

Where, λ_1 and λ_2 are similar to each other so that it is assumed that they are identical to each other.

The cycle of the measured signal 68 is varied by Doppler effect according to a moving speed and movement direction of the moving reflecting mirror 63 whereas the cycle of the reference signal 76 is uniform. The displacement of the moving object to which the moving reflecting mirror is attached can be measured by continuously measuring a relative phase difference between the reference signal and the measured signal.

A measurement resolution is determined according to a degree of resolution of the phase difference between the two signals. As described above, the heterogeneous mode helium-neon laser has two modes and its resonator has a length of 150 to 200mm. The distance between the two modes is determined by a free spectral range. The distance depends on the length of the resonator but is in the range of

600 to 1000MHz in general. If the wavelength of laser beam is 633nm, in order to obtain the measurement resolution of 0.1nm, the phase measuring resolution of $2 \times 360^\circ \times (0.1\text{nm}) / 633\text{nm} = 0.1^\circ$ is required when the Expression 9 is applied. However, this small phase is difficult to directly measure using a phase meter. To solve this problem, the present invention reduces the frequencies of the reference signal and the measured signal without changing the phases of the two signals by using a super heterodyne technique, to thereby enable phase measurement even if beat frequencies of the signals are high.

A method capable of increasing the measurement resolution will be explained below.

A local oscillator 82 artificially creates a local signal 87 approximate to the beat frequency corresponding to the reference signal. To apply the local signal to the measured signal and the reference signal, a signal splitter 83 splits the local signal 87 into two signals 88 and 89. Though it is desired that the local signal 87 be different from the beat frequency by 1MHz to 20MHz, it is determined according to the configuration of the system. Mixers 86 and 81 multiply the split signals 88 and 89 by the reference signal 76 and the measured signal 68, respectively. The mixers 86 and 81 output signals 91 and 92 corresponding to the sums of the frequencies of the multiplied two signals and the differences of the frequencies of the multiplied two signals. The signals corresponding to the sums are eliminated by filters

84 and 85. Outputs 93 and 94 of the filters 84 and 85 are inputted to a phase meter 100 to measure their phases. The reference signal 93 and the measured signal 94 whose frequencies are reduced can be represented as follows.

$$V_m' = A \cos 2\pi f t \quad (\text{Expression 10})$$

$$V_m' = B \cos \{2\pi (f t + 2nd_1 / \lambda_1 - 2nd_2 / \lambda_2)\} \quad (\text{Expression 11})$$

Where, $f = f_1 - f_2 - f_{LO}$ where f_{LO} is the frequency of a local oscillation signal. When f_{LO} is set similar to the beat frequency, the beat signal frequency can be reduced to the measuring band of the phase measurer. Since f_{LO} can be varied, the frequencies of the reference signal and the measured signal can be controlled according to a speed and a resolution of an object to be measured. A heterogeneous mode laser outputs power of more than 2mW. Accordingly, if efficiency of the plane mirror interferometer is 60% and a minimum measurable light intensity is 50mW, the interferometer can measure at least 20 axes when the heterogeneous mode laser is used as a light source of the interferometer.

[01] When the reference signal frequency is reduced, however, the measuring band is limited. FIG. 4A shows the measuring band when the beat frequency is not decreased, in which the bandwidth in the case 110 where Doppler frequency operates in a positive direction is the same as the bandwidth in the case 111 where the Doppler frequency

operates in a negative direction. When the beat frequency is reduced, although a band 112 is not varied when the Doppler frequency operates in the positive direction, a measuring band 113 becomes narrow in the negative direction, as shown in FIG. 4B. To solve this, the present invention uses a two-way heterodyne technique.

FIG. 4C shows an embodiment of the two-way heterodyne technique. A signal splitter 116 splits a measured signal 115 into two signals 121 and 122. Two mixers 117 and 118 multiply the split signals 121 and 122 by a local oscillation signal 123 whose frequency is $f_b + f$ and a local oscillation signal 124 whose frequency is $f_b - f$, respectively. Where, f_b means a beat frequency.

Radio frequency components of outputs 125 and 126 of the mixers are eliminated by filters 119 and 120. The filters respectively output a signal 127 having a frequency $f + \Delta f$ and a signal 128 having a frequency $f - \Delta f$. Phase measurers 130 and 131 measure Doppler frequency. If the signal 127 whose frequency is $f + \Delta f$ and a measured value of the phase measurer 130 are used when the Doppler frequency has the positive sign and the signal 128 whose frequency is $f - \Delta f$ and a measured value of the phase measurer 131 are used when it has the negative sign, a band in the positive direction is used all the time so that the same band can be used irrespective of the sign of the Doppler frequency. Since the two phase measurers 130 and 131 are employed, the phase measurers are changed when the movement direction of the

object is varied, and phase values of the phase measurers are exchanged when the phase measurers are changed, so as to prevent loss of phase even when a measuring direction is varied.

The heterodyne interferometer is a well-known displacement measuring device widely used. Accordingly, constitutions and methods, which are not included in the claims of the present invention, can be easily embodied by those skilled in the art from the well-known heterodyne interferometer so that detailed explanation for them is omitted.

While the present invention has been described with reference to the particular illustrative embodiments, it is not to be restricted by the embodiments but only by the appended claimed. It is to be appreciated that those skilled in the art can change or modify the embodiments without departing from the scope and spirit of the present invention.

What is claimed is:

1. A heterodyne laser interferometer using a heterogeneous mode helium-neon laser and a super heterodyne phase measuring method, comprising a laser light source part 70, an optical interferometer 60, a frequency converter 80 and a phase measurer 90,

wherein the laser light source part uses a heterogeneous mode helium-neon laser generator 71, output light emitted from the laser generator has two frequencies that are perpendicular to each other and linearly polarized, a part 75 of the output light is used as a reference signal and the remaining output light 74 is used as a measured signal.

2. The heterodyne laser interferometer as claimed in claim 1, wherein the reference signal is obtained in such a manner that a part of the output light passes through a polarizer 72 whose polarization axis is tilted at 45° to the light having two frequencies to interfere and then passes through a photo-detector 73 to be converted into an electric signal 76, the reference signal being represented by

$$V_r = A \cos[2\pi(f_1 - f_2)t]$$

where V_R is the reference signal, A is the amplitude of the signal, and f_1 and f_2 are frequency components included in the output light.

3. The heterodyne laser interferometer as claimed in claim 1, wherein the measured signal is obtained in such a manner that the remaining output light is inputted into a polarization splitter 62 to be split so that light 67 having a frequency component f_1 travels to a fixed reflecting mirror 61 and light 66 having a frequency component f_2 travels to a moving reflecting mirror 63 attached to a moving object, the lights inputted into the fixed reflecting mirror and the moving reflecting mirror are reflected and combined by a polarizer 64 whose polarization axis is tilted at 45° to the lights to interfere with each other, the combined light is inputted to a photo-detector 65, and the light inputted into the photo-detector is converted into an electric signal, the measured signal being represented by

$$V_m = B \cos\{2\pi(f_1 - f_2)t + 2nd_1 / \lambda_1 - 2nd_2 / \lambda_2\}$$

where V_m is the measured signal, B is the amplitude of the signal, λ_1 and λ_2 mean wavelengths of the lights having the frequency components f_1 and f_2 , respectively, d_1 is a distance that the light having the frequency component f_1 has traveled in the air, d_2 is a distance that the light having the frequency component f_2 has traveled in the air, and n is the reflective index of air.

4. The heterodyne laser interferometer as claimed in claim 1, wherein a local oscillator 82 creates a local signal 87 approximate to a beat frequency corresponding to the reference signal, a signal splitter 83 splits the local signal 87 into two signals 88 and 89, mixers 86 and 81 multiply the split signals 88 and 89 by the reference signal 76 and the measured signal 68, respectively, a filter

84 eliminates a signal corresponding to the sum of the reference signal and the local signal among the output signal 91 of the mixer that multiplies the reference signal by the local signal, a phase meter 100 receives a signal corresponding to the difference of the reference signal and the local signal, a filter 85 eliminates a signal corresponding to the sum of the measured signal and the local signal among the output signal 92 of the mixer that multiplies the measured signal by the local signal, the phase meter 100 accepts a signal corresponding to the difference of the measured signal and the local signal, to thereby measure a phase.

5. The heterodyne laser interferometer as claimed in claim 4, wherein the signal corresponding to the difference of the reference signal and the local signal is represented by

$$V_m' = A \cos 2\pi f t$$

and the signal corresponding to the difference of the measured signal and the local signal is represented by

$$V_m' = B \cos \{2\pi (f t + 2n d_1 / \lambda_1 - 2n d_2 / \lambda_2)\}$$

where $f = f_1 - f_2 - f_{LO}$, f_{LO} is the frequency of a local oscillation signal, f_1 and f_2 are frequency components included in output lights, λ_1 and λ_2 mean wavelengths of the lights having the frequency components f_1 and f_2 , respectively, d_1 is a distance that the light having the frequency component f_1 has traveled in the air, d_2 is a distance that the light having the frequency component f_2 has traveled in the air, and n is the reflective index of air.

6. The heterodyne laser interferometer as claimed in claim 3, wherein a signal splitter 116 splits a measured signal 115, which was converted into an electric signal, into two signals 121 and 122, a mixer 117 multiplies one of the split signals 121 and 122 by a local oscillation signal 123 whose frequency is $f_b + f$, a mixer 118 multiplies the other signal 122 by a local oscillation signal 124 whose frequency is $f_b - f$, radio frequency components of outputs 125 and 126 of the mixers are eliminated by filters 119 and 120, to generate a signal 127 having a frequency $f + \Delta f$ and a signal 128 having a frequency $f - \Delta f$, phase measurement is carried out using the signal 127 having the frequency $f + \Delta f$ when Doppler frequency has a positive sign, and phase measurement is performed using the signal 128 having the frequency $f - \Delta f$ when the Doppler frequency has a negative sign.

7. A heterodyne laser interferometer using a heterogeneous mode helium-neon laser and a super heterodyne phase measuring method, comprising a laser light source part 70, an optical interferometer 60, a frequency converter 80 and a phase measurer 90,

wherein the laser light source part uses a heterogeneous mode helium-neon laser generator 71, output light emitted from the laser generator has two frequencies that are perpendicular to each other and linearly polarized, a part 75 of the output light is used as a reference signal and the remaining output light 74 is used as a measured signal.

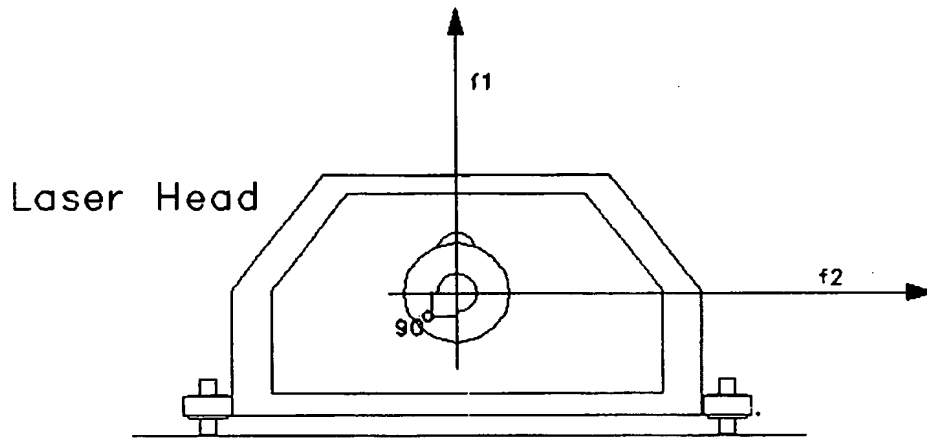
the reference signal is obtained in such a manner that a part of the output light passes through a polarizer 72 whose polarization axis is tilted at 45° to the light having two frequencies to interfere and then passes through a photo-detector 73 to be converted into an electric signal 76.

the measured signal is obtained in such a manner that the remaining output light is inputted into a polarization splitter 62 to be split so that light 67 having a frequency component f_1 travels to a fixed reflecting mirror 61 and light 66 having a frequency component f_2 travels to a moving reflecting mirror 63 attached to a moving object, the lights inputted into the fixed reflecting mirror and the moving reflecting mirror are reflected and combined by a polarizer 64 whose polarization axis is tilted at 45° to the lights to interfere with each other, the combined light is inputted to a photo-detector 65, and the light inputted into the photo-detector is converted into an electric signal,

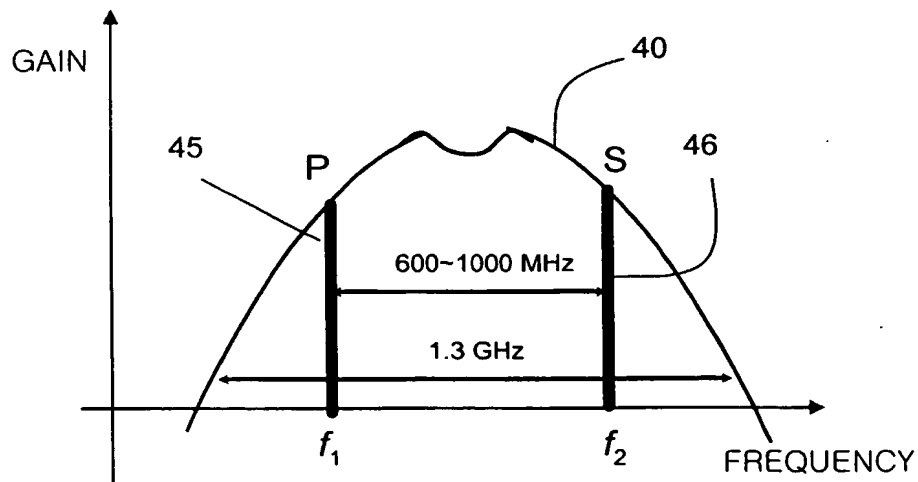
a local oscillator 82 creates a local signal 87 approximate to a beat frequency corresponding to the reference signal, a signal splitter 83 splits the local signal 87 into two signals 88 and 89, mixers 86 and 81 multiply the split signals 88 and 89 by the reference signal 76 and the measured signal 68, respectively, a filter 84 eliminates a signal corresponding to the sum of the reference signal and the local signal among the output signal 91 of the mixer that multiplies the reference signal by the local signal, a phase meter 100 receives a signal corresponding to the difference of the reference signal and the local signal, a filter 85 eliminates a signal corresponding to the sum of the measured signal and the local signal among the output signal 92 of the mixer

that multiplies the measured signal by the local signal, the phase meter 100 accepts a signal corresponding to the difference of the measured signal and the local signal, to thereby measure a phase.

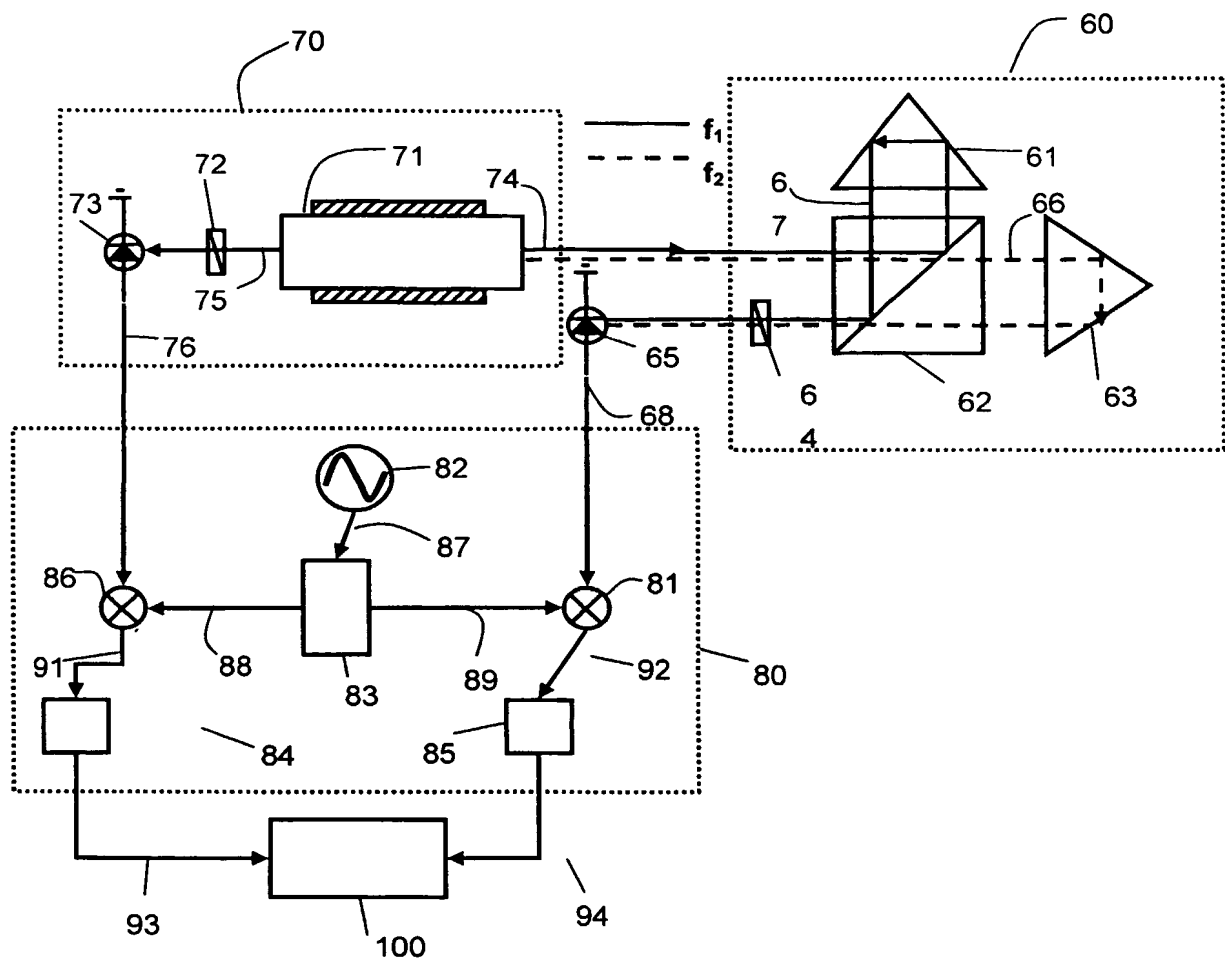
【FIG 1】



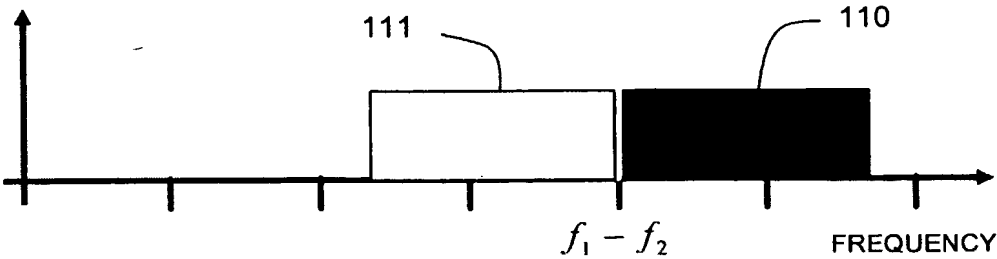
【FIG 2】



【FIG 3】



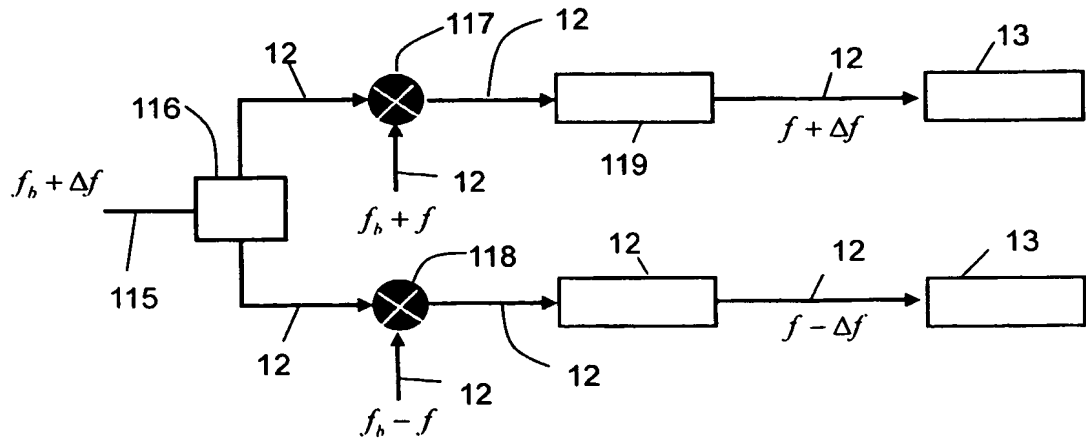
【FIG 4a】



【FIG 4b】



【FIG 4c】



INTERNATIONAL SEARCH REPORT

International application No.

PCT/KR02/01330

A. CLASSIFICATION OF SUBJECT MATTER

IPC7 G01N 21/45

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC7 G01B 9/02, G01B 11/00

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Korean patents and applications for inventions since 1975, Korean utility models and applications for utility models since 1975
Japanese utility models and applications for utility models since 1975

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

NPS, JPO

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 5,677,768 A (Hewlett-Packard Company) 14 Oct. 1997 see the abstract and figure 1	1
Y	JP 2001-156361 A (YOKOYAMASHIYUUKO) 8 Jun. 2001 see the whole document	1
A	US 5,106,191 A (Canon Kabushiki Kaisha) 21 Apr. 1992 see the whole document	1-7
A	US 5,579,109 A (Korea Research Institute of Standards and Science) 26 Nov. 1996 see the whole document	1-7
A	US 4,498,773 A (Rockwell International Corp.) 12 Feb. 1985 see the whole document	1-7
A	KR 2001-37162 A (Yun-chang, Park) 7 May 2001	1-7

☐ Further documents are listed in the continuation of Box C.

☐ See patent family annex.

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Date of the actual completion of the international search

27 MARCH 2003 (27.03.2003)

Date of mailing of the international search report

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